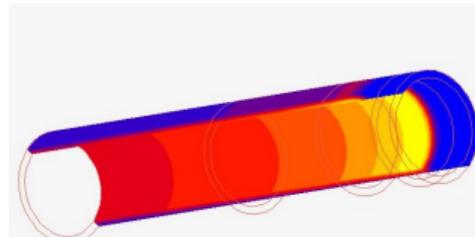


Cyclic plasticity's models for thermo-mechanical applications. Case of a copper mold for continuous casting

Marco Andreola

Supervisors: Francesco De Bona

Jelena Srnec Novak



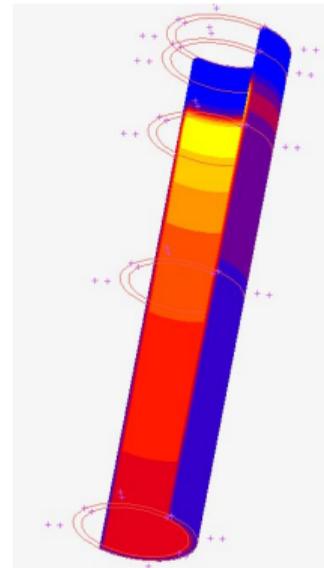
Summary

- ▶ Introduction
 - ▶ Presentation of the case studied
 - ▶ Cyclic behavior of materials
- ▶ Case study
 - ▶ Thermo-mechanical application of the mold through:
 - ▶ Combined model
 - ▶ Accelerated model
 - ▶ Stabilized model
 - ▶ Linear kinematic model
- ▶ Fatigue life assessment
- ▶ Conclusions

Introduction

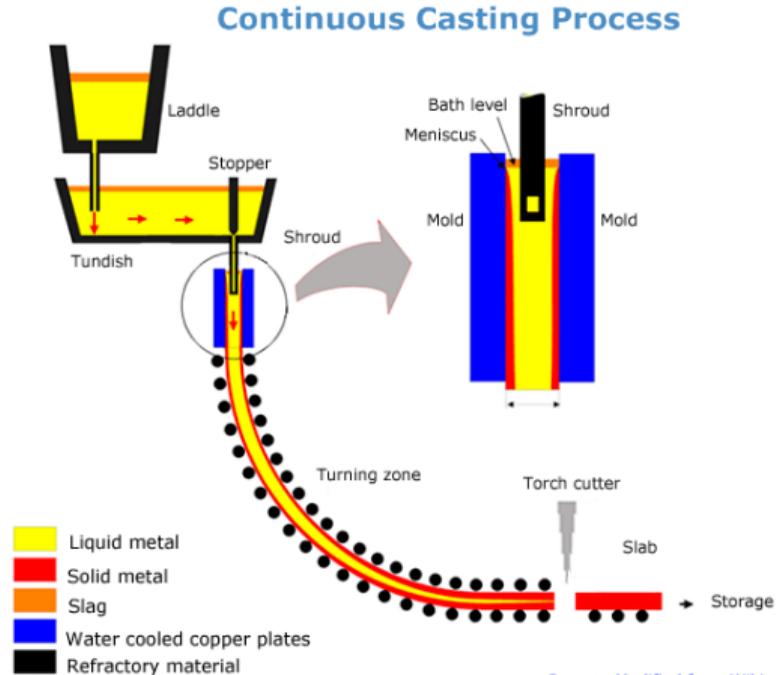
Several mechanical components work undergoing high stresses, cyclic loading, high temperature etc. The procedure adopted is

- ▶ Analyze results obtained from different material model using Marc Mentat to analyze thermal-structural behavior.
- ▶ Assess service life of a copper-silver mold.
- ▶ Find the most suitable model in terms of solution's reliability and time employed;



Case study: the copper-silver mold

Copper-silver mold is a key component for the continuous casting.



Source: Modified from Wikipedia

Material behavior

Main concepts:

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- ▶ The goal is to **find appropriate material models** which are able to simulate behavior very similarly with experimental data.
- ▶ **Different materials** under cyclic loading **behave in different ways**;
- ▶ **So far**, many researchers aimed to describe cyclic behavior for different materials, thereby developing **several constitutive equations**;

Main hardening models

The most important are able to capture some physical features through description of the yield surface.

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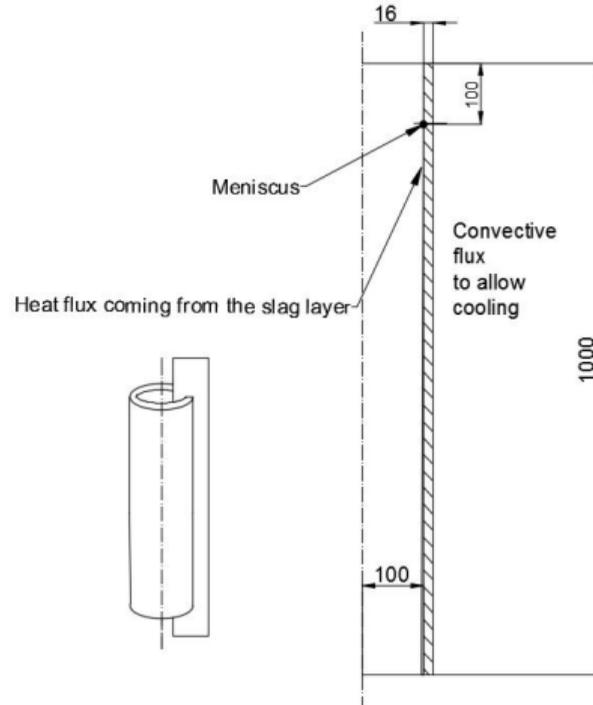
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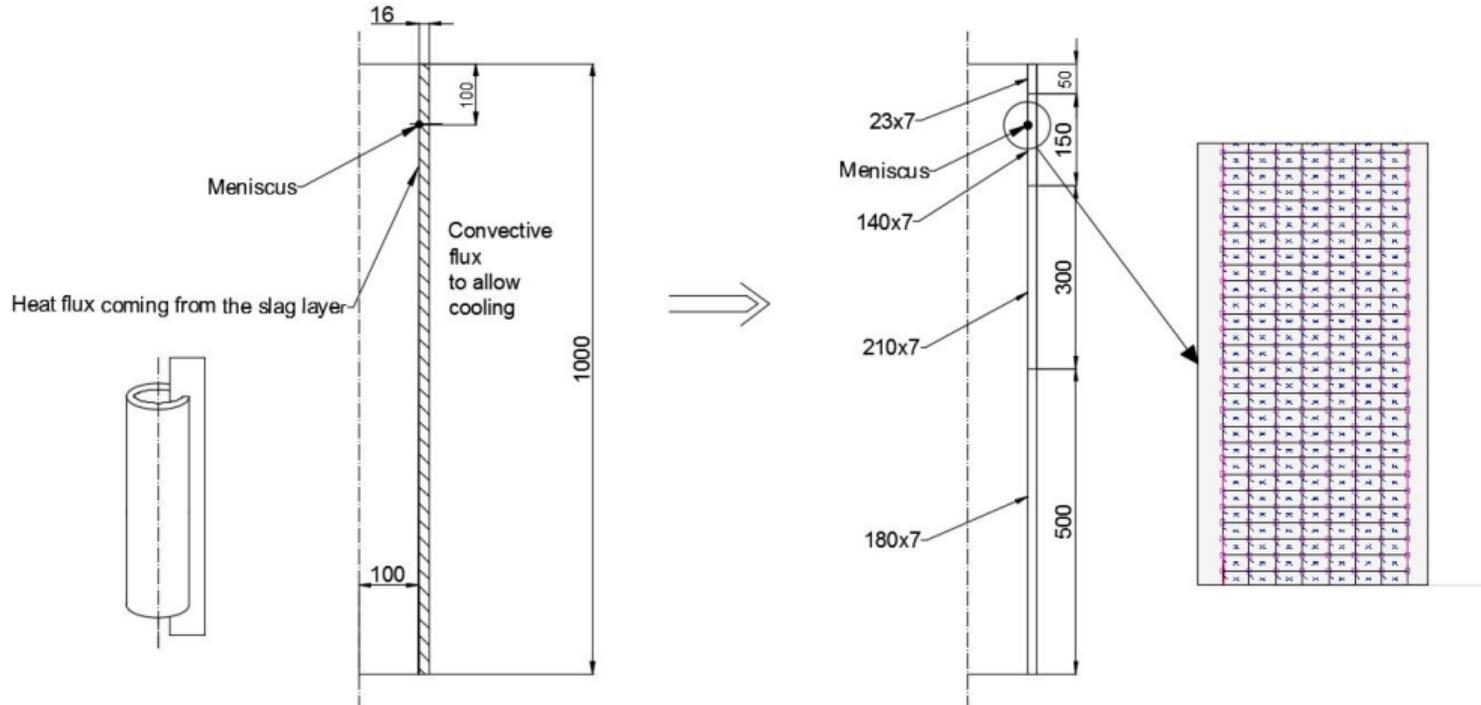
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- ▶ Combined \Rightarrow Isotropic + Kinematic

Model definition: Geometry [Galdiz,2014] and mesh



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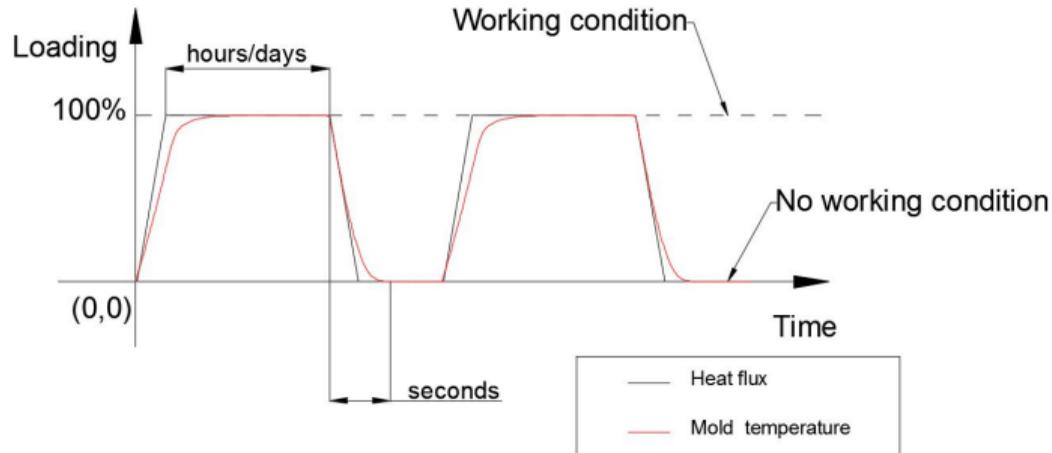


Modeling

- ▶ Material properties [Novak, 2013], are adopted for a combined model;

Temp. [°C]	E[GPa]	σ_{y0} [MPa]	C [MPa]	γ [MPa]	R_{∞} [MPa]	b
20	119	130	42 250	617	-75.7	2.35
250	104	111	45 340	820	-80.2	3.89
300	103	110	40 080	832	-76.7	5.29

- ▶ Boundary conditions [Galdiz,2014] are required to simulate the working conditions;

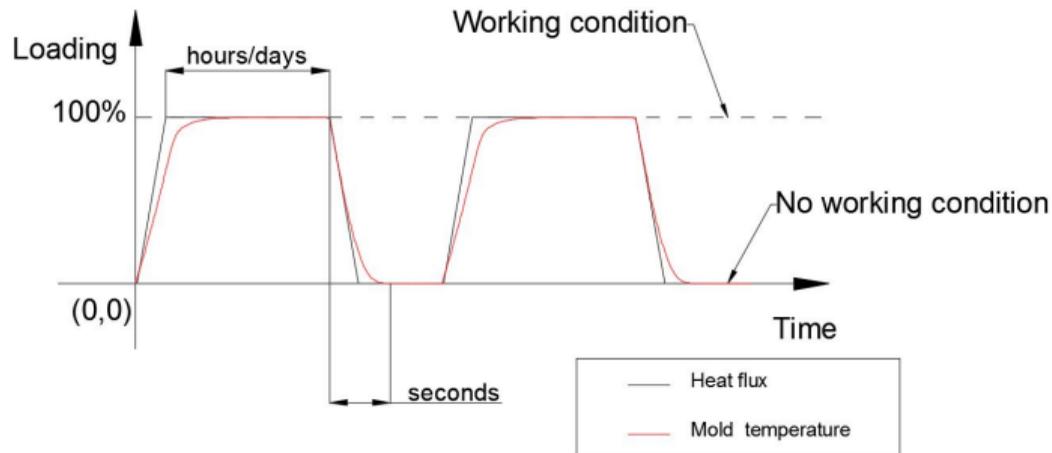


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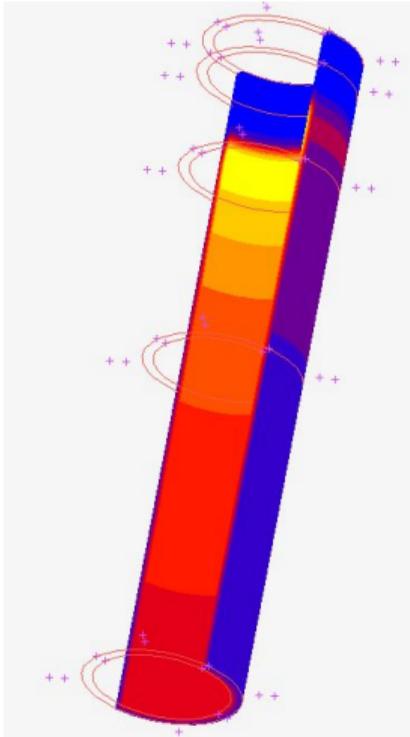
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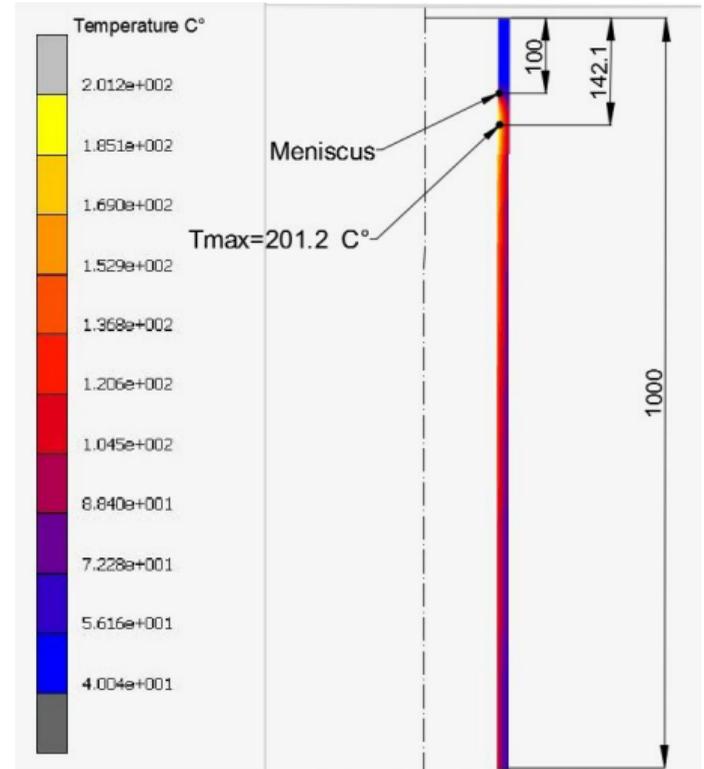
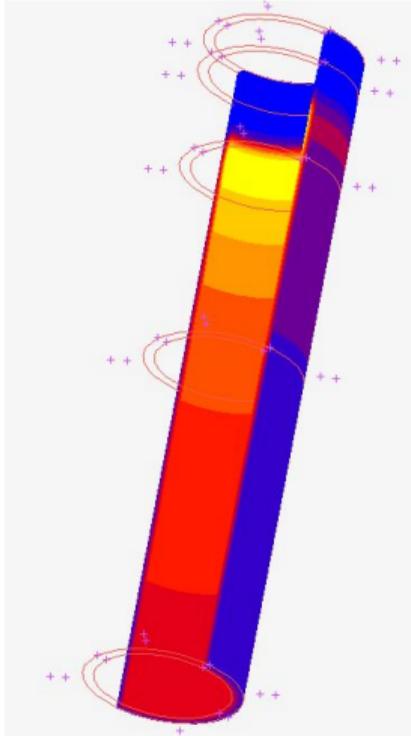
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Temperature field

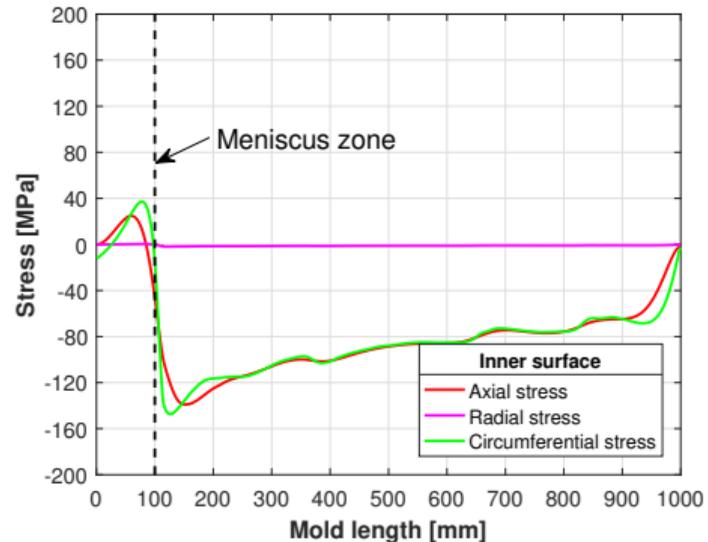
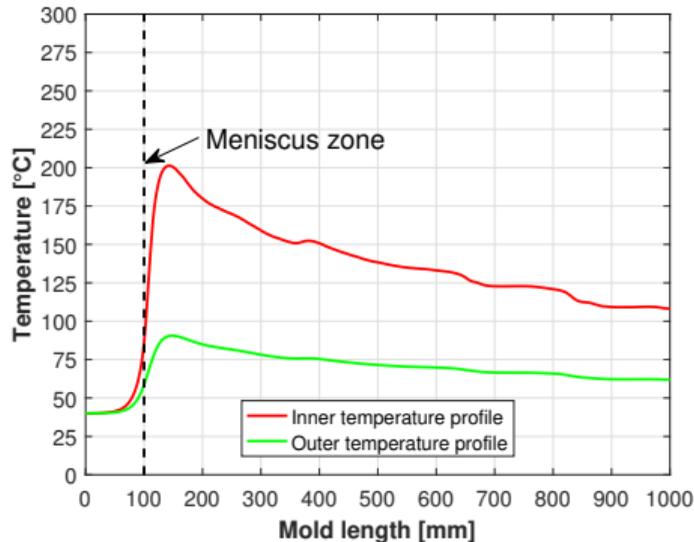


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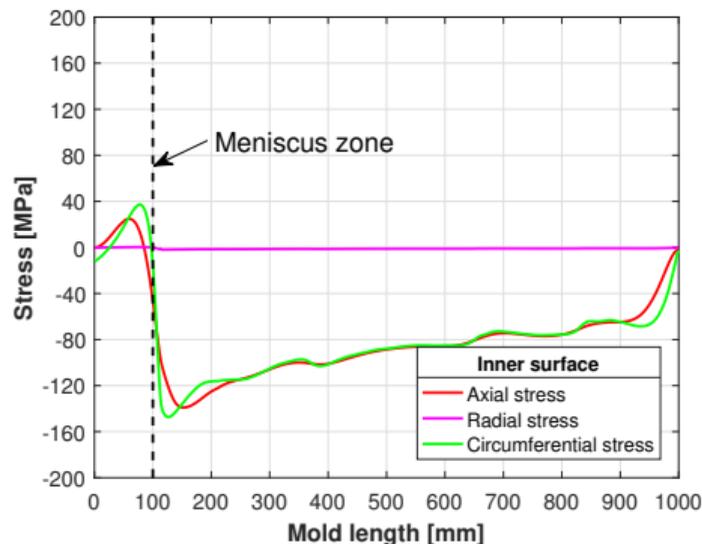
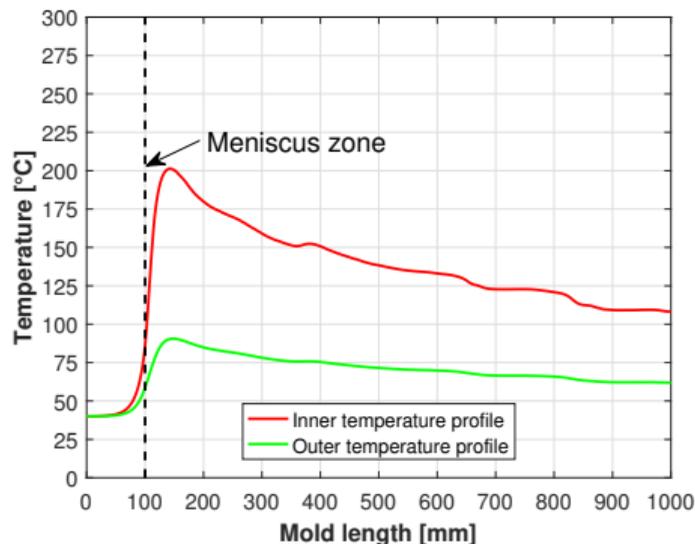
Temperatures and stresses distribution

- ▶ Temperatures profile; Stress profiles in the inner surface;



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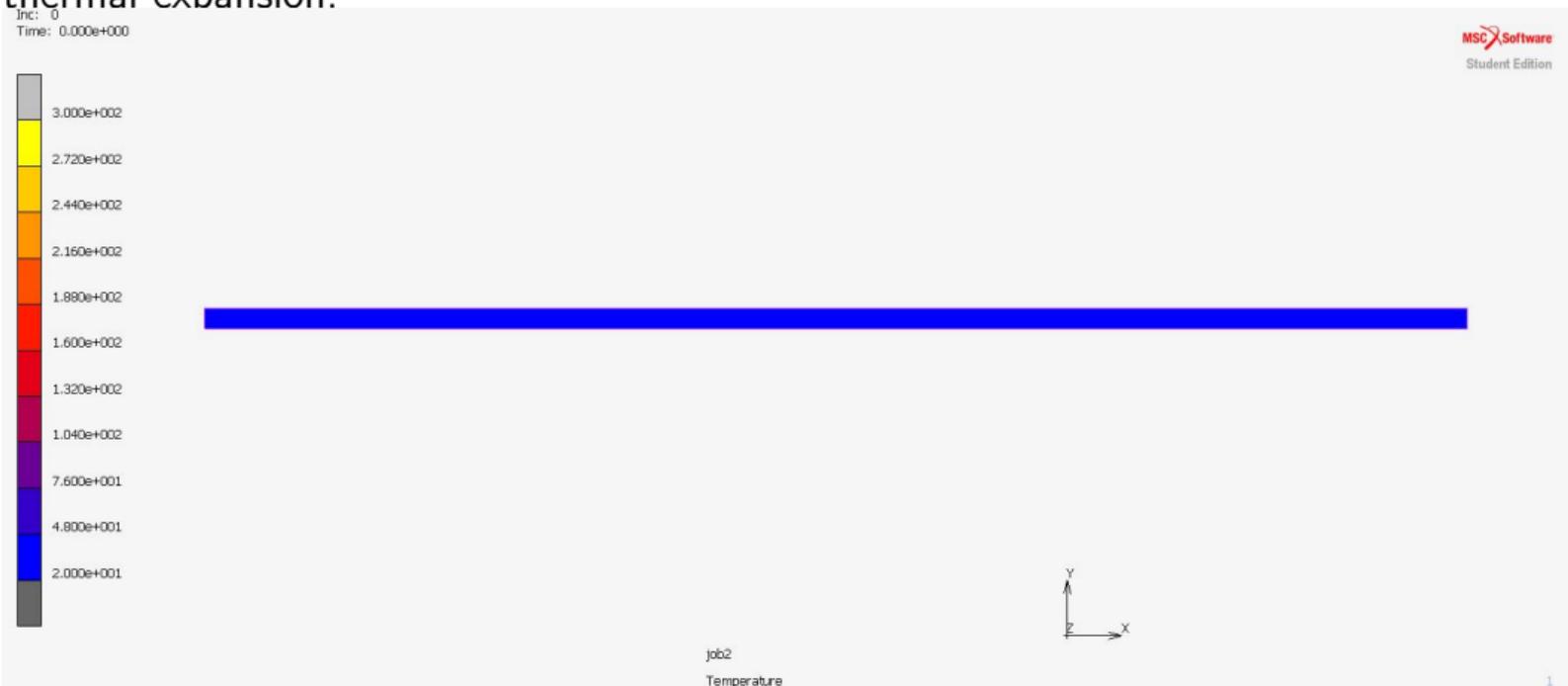
- ▶ Temperatures profile; Stress profiles in the inner surface;



- ▶ The critic point is where the maximum temperature occurs [Mahapatra,1991];

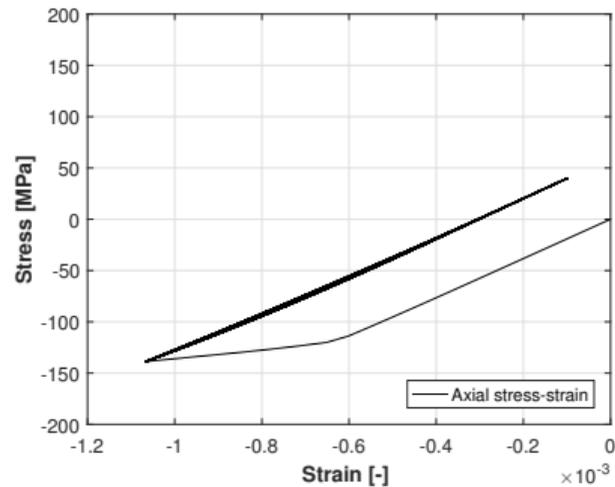
Thermo-structural behavior

The profile plotted supplies temperature field, with the deformations determined by thermal expansion.



Stress-strain curves

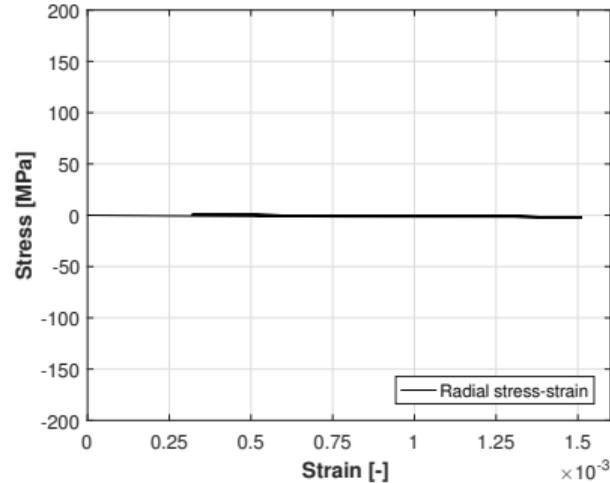
After the first cycle, in each direction the stress is not able to overcome the actual yield stress arisen.



In order to assess different material models, it has been chosen to increase the thermal flux.

Stress-strain curves

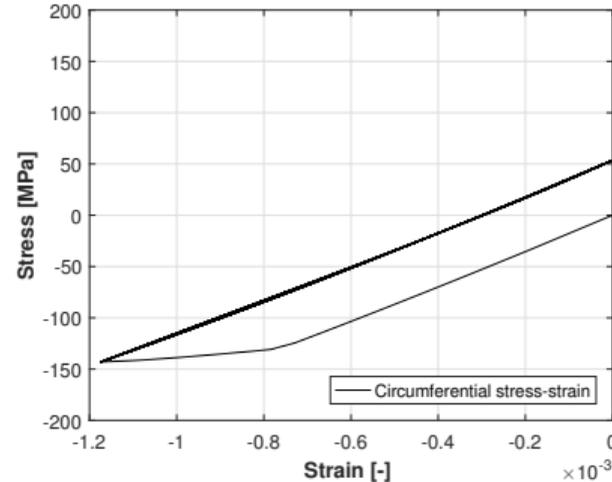
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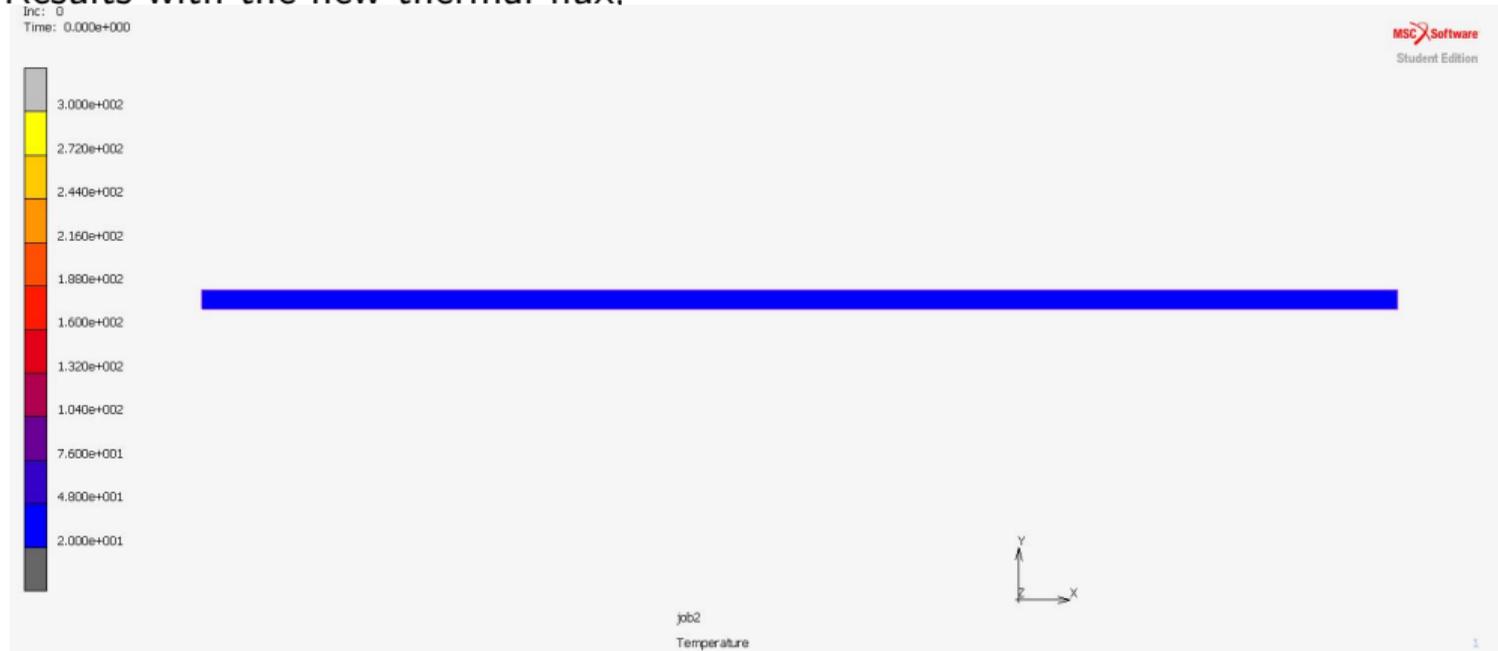
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Thermo-structural behavior

- ▶ Results with the new thermal flux:



Cyclic behavior

- ▶ Analysis of cyclic behavior aims to find **stabilized conditions**;
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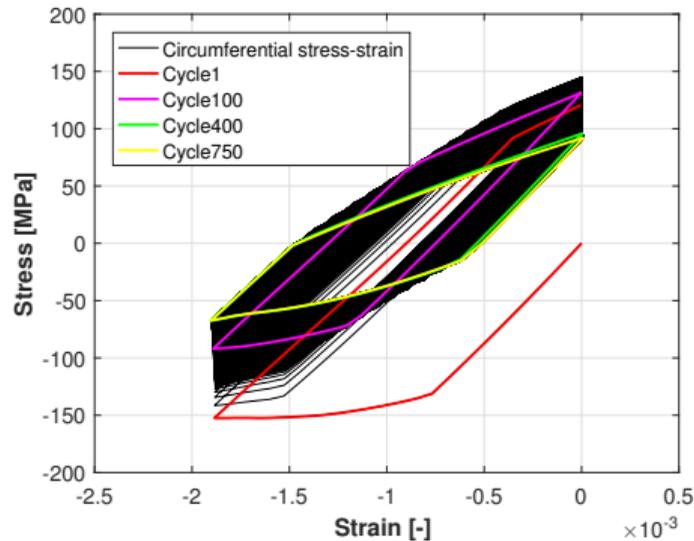
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 - ▶ Stabilized.
 - ▶ Linear kinematic or Prager's model;
- ▶ In order to determine the number of cycles to reach stabilization, an empiric formula has been used [Lemaitre,Chaboche,1994]: $2bN\Delta\varepsilon_{pl} \approx 5$
- ▶ In order to determine uniquely stabilized conditions it is used this own criterion.
 $((\Delta\varepsilon_{pl,n+10} - \Delta\varepsilon_{pl,n})/\Delta\varepsilon_{pl,n})100 < 0.35$

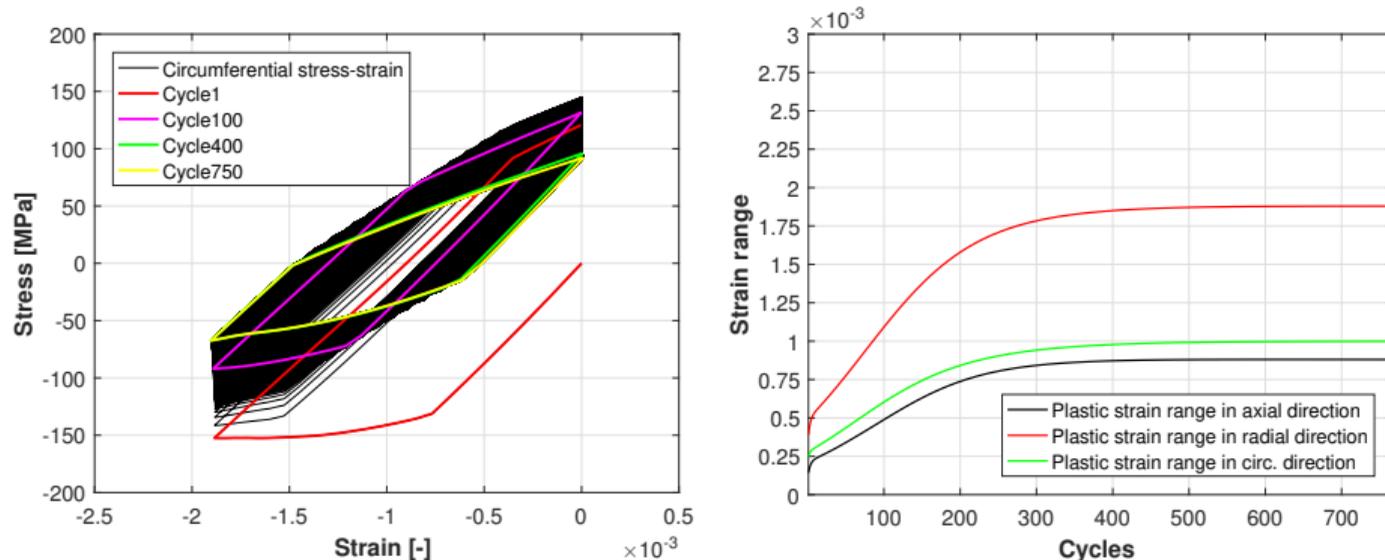
Results with the combined model

Cyclic behavior in circumferential direction: stress strain curve and plastic strain range behavior. This model supplies the best results with experimental data.



Results with the combined model

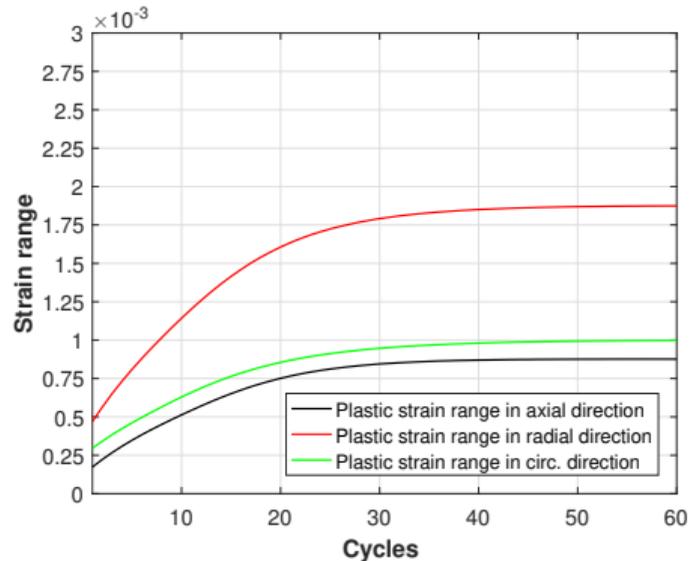
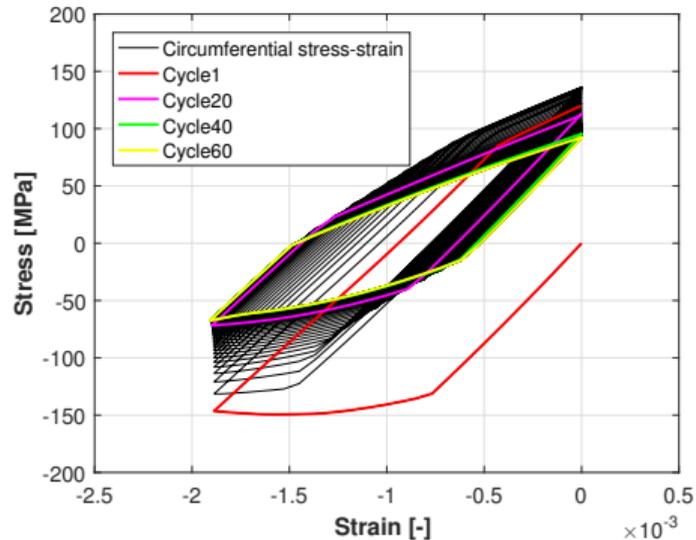
Cyclic behavior in circumferential direction: stress strain curve and plastic strain range behavior. This model supplies the best results with experimental data.



Here 750 cycles are plotted, the solver took $36\,715s \approx 10\text{ h}$; stabilization is reached after 349 cycles.

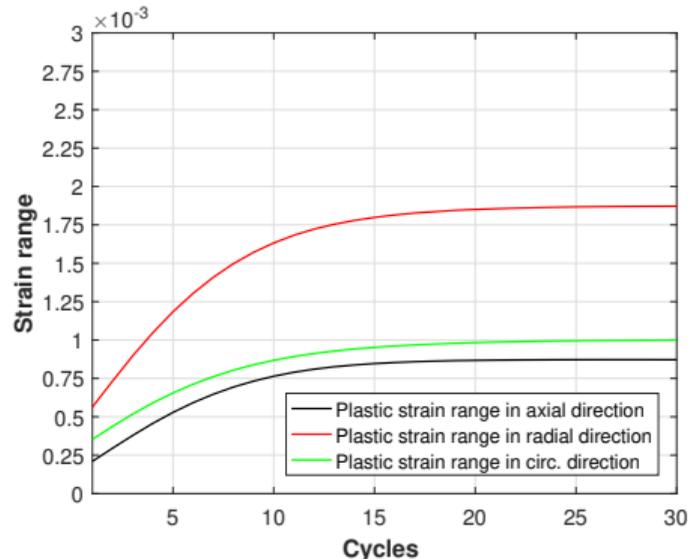
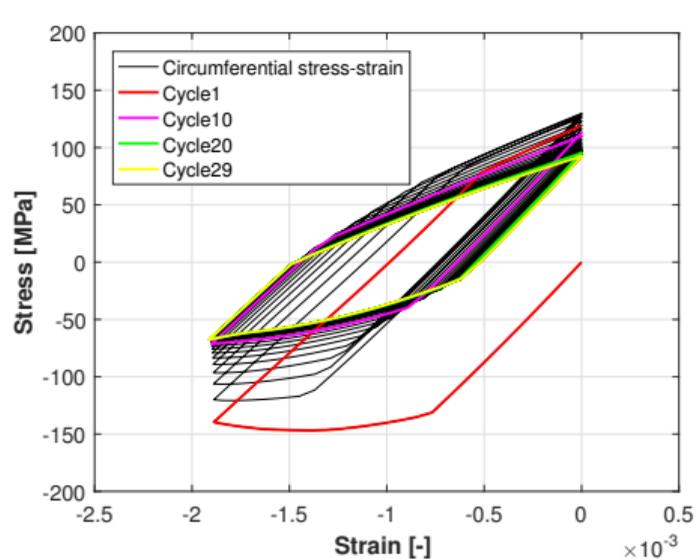
Accelerated model with $b = 10b_i$

Such model allows a great reduction of the number of cycle to obtain stabilization.



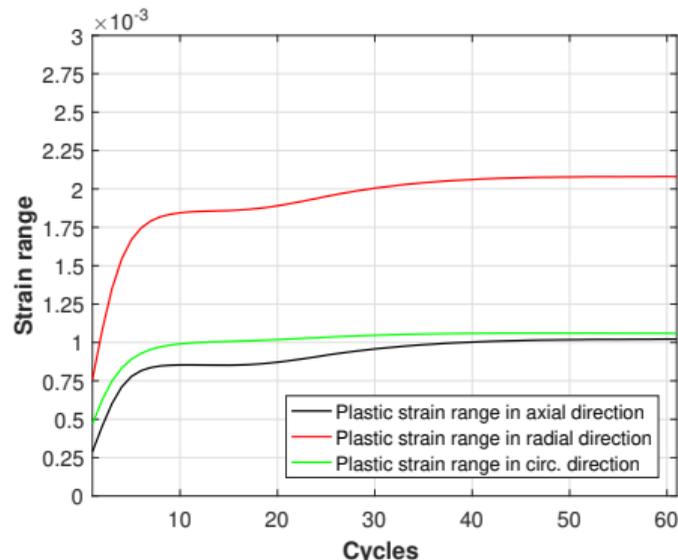
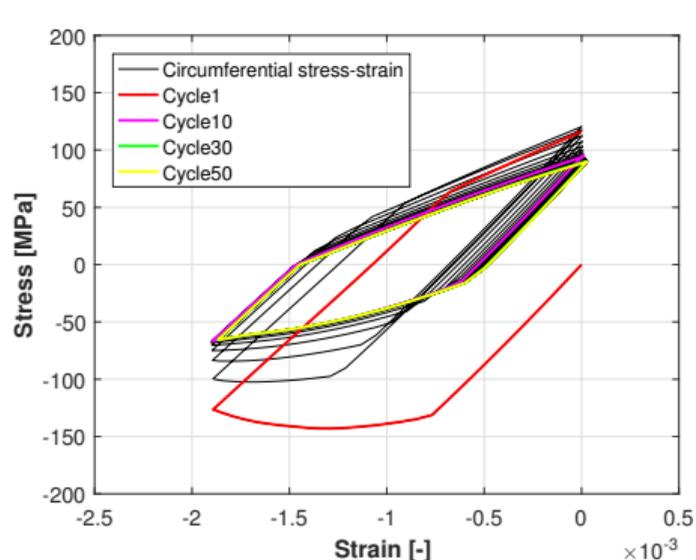
Here 60 cycles are plotted, the solver took 2 266 s (comparing with the first case **time reduction** is **93.8%**); stabilization is reached after 58 cycles.

Accelerated model with $b = 20b_i$



Here 30 cycles are plotted, the solver took 1 136 s (comparing with the first case **time reduction is 96.9%**); stabilization is reached after 28 cycles.

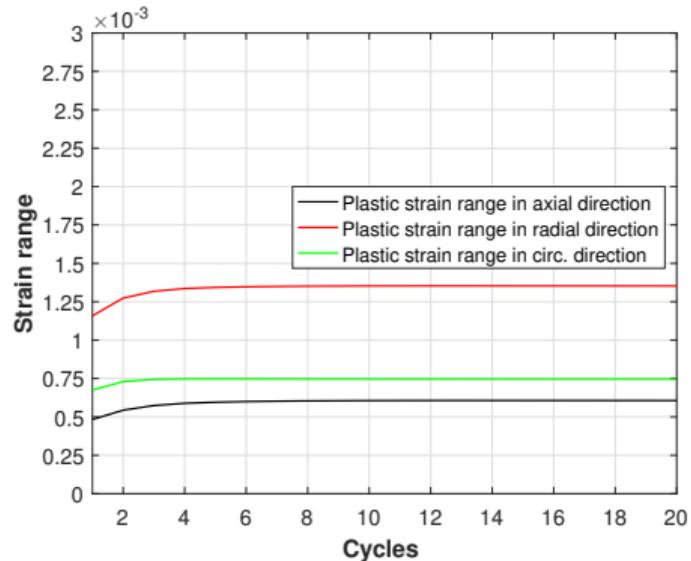
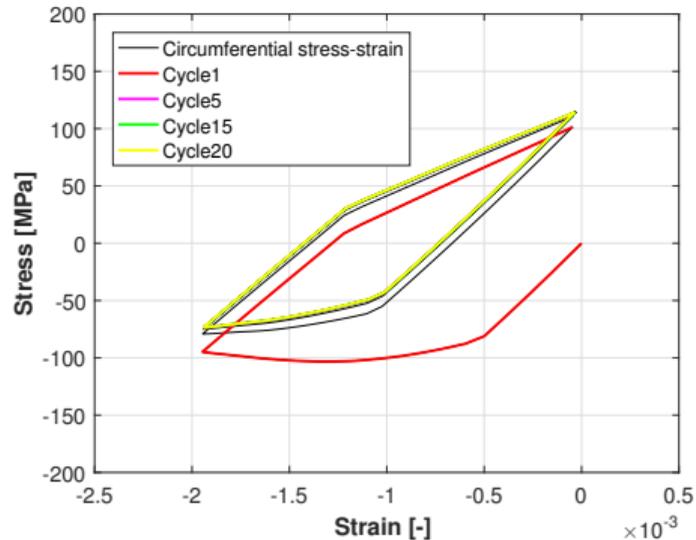
Accelerated model with $b = 40b_i$



Here 60 cycles are plotted, the solver took 2 560 s (comparing with the first case **time reduction is 93.0%**); stabilization is reached after 51 cycles.

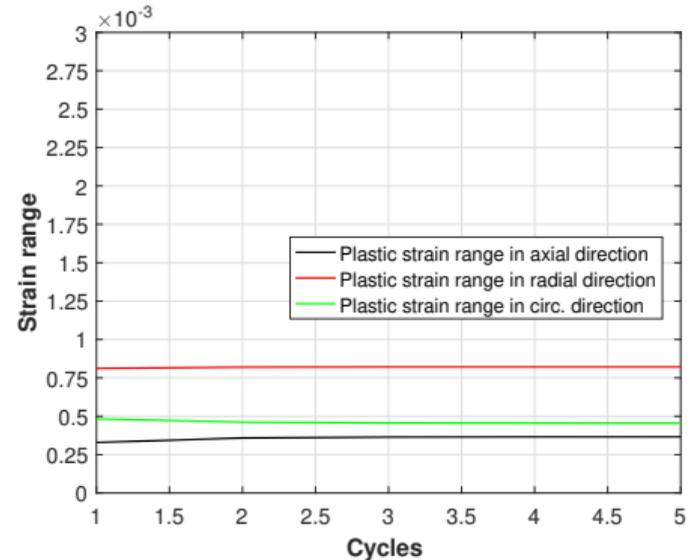
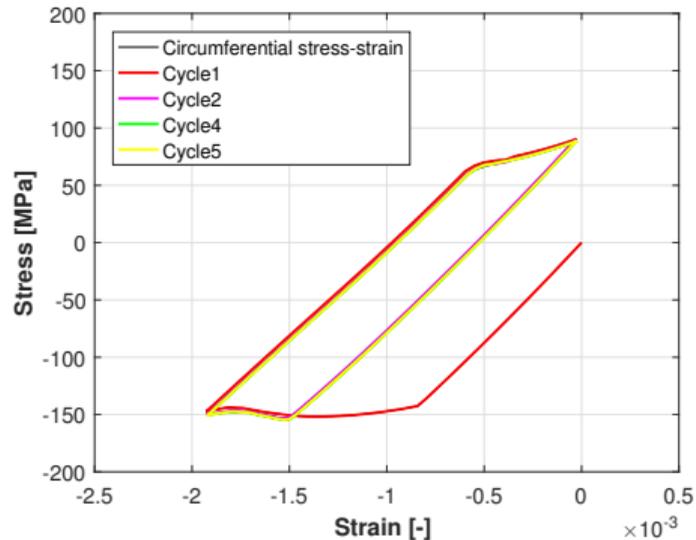
Stabilized model

It exploits material data from stabilized conditions, it is a non linear kinematic model.



Here 20 cycles are plotted, the solver took 534 s (comparing with the first case **time reduction** is **98.5%**); stabilization is reached after 11 cycles.

Linear kinematic model



Here 5 cycles are plotted, the solver took 1 002 s (comparing with the first case **time reduction is 97.3%**); stabilization is reached after 3 cycles.

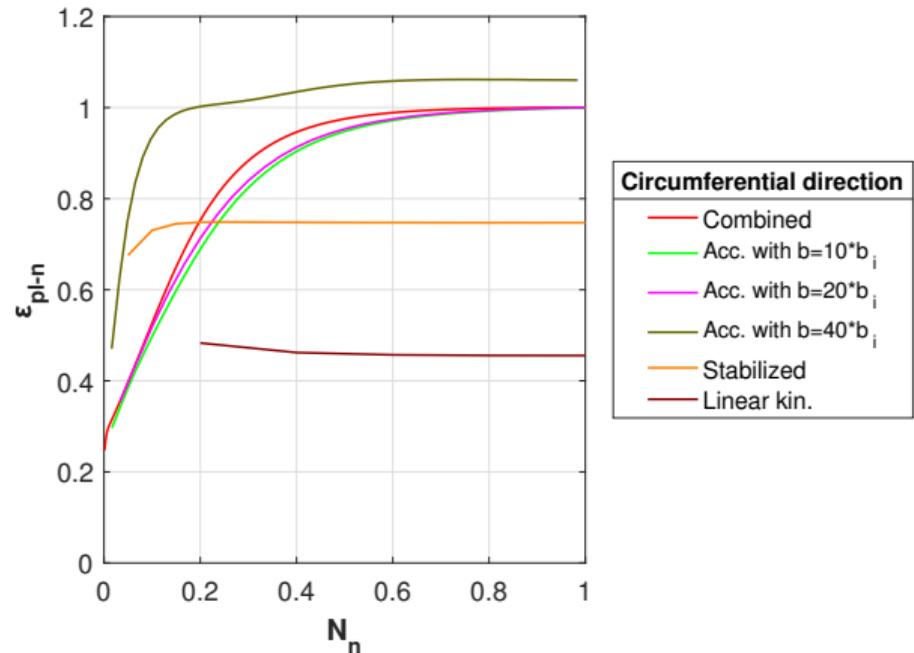
Comparison of plastic strain range

Normalizing the number of cycles and the plastic strain range, a comparison can be done.

- ▶ Considering the i^{th} model

$$\text{It has } N_n^i = \frac{N^i}{N_{stab}^i}$$

$$\text{and } \varepsilon_{pl-n} = \frac{\Delta\varepsilon_{pl}^i}{\Delta\varepsilon_{pl,750,comb.model}}$$



Cycles needed to reach stabilization

Now these steps are followed:

- ▶ Number of cycles to obtain the stabilization are determined;
- ▶ It has been listed the time employed by the solver;

Material model	Cycles computed	Time [s]	Cycles to stab.	Time to reach stabilization [s]	% Time saved
Combined	750	36 715	349	17 085	—
Acc. $b = 10 * b_i$	60	2 266	58	2 577	84.9
Acc. $b = 20 * b_i$	30	1 136	28	1060	93.8
Acc. $b = 40 * b_i$	60	2 560	51	2 176	87.3
Stabilized	20	534	11	294	98.2
Linear kin.	5	1 002	3	601	96.5

Fatigue life assessment

Now, fatigue life assessment can be carried out

- ▶ Evaluation of equivalent strain range
[Manson, 2009] $\rightarrow \Delta\varepsilon_{eq}$.

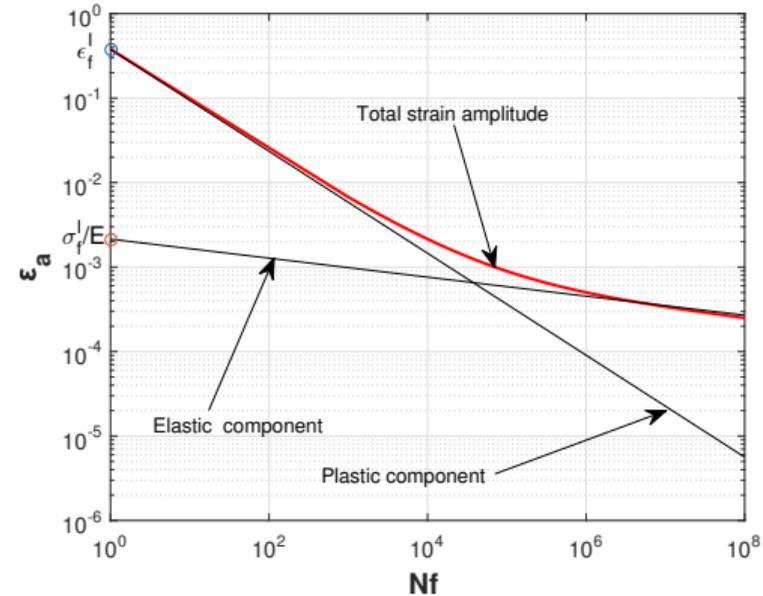
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- ▶ Evaluation of equivalent strain range [Manson, 2009] $\rightarrow \Delta \varepsilon_{eq}$.
- ▶ Determination of material properties
 \Rightarrow [Novak, 2013]
 \Rightarrow Manson-Coffin-Basquin curve



- ▶ N_f : **Number of cycles to failure;**



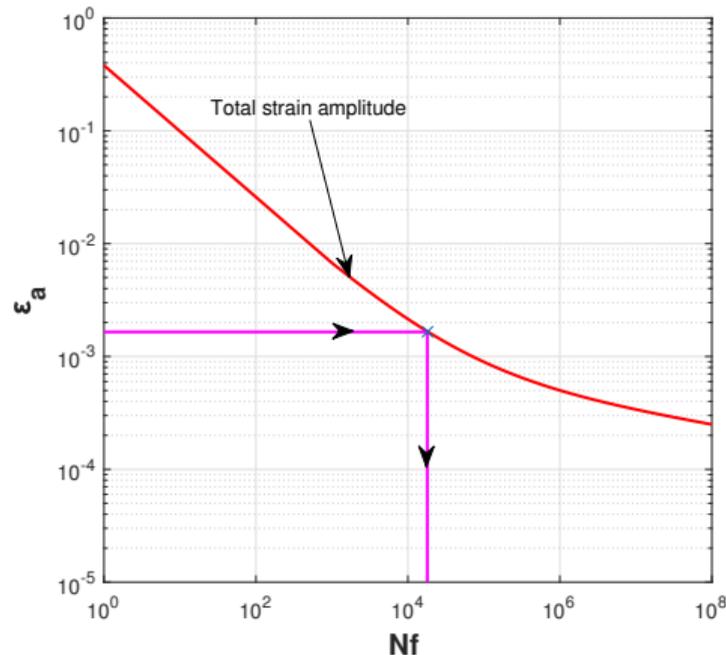
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Fatigue life assessment

Material model	$\Delta\varepsilon_{eq}$ $\cdot 10^{-3}$	Life assessment [<i>Cycles</i>]	$\Delta\varepsilon_{rl}$ [%]	% Time saved
Combined	3.16	20 461	–	–
Acc. with $b = 10 * b_i$	3.16	20 571	+0.5	84.9
 Acc. with $b = 20 * b_i$	3.15	20 631	+0.8	93.8
Acc. with $b = 40 * b_i$	3.31	18 261	–10.8	87.3
Stabilized	2.98	23 791	+16.3	98.2
Linear kinematic	2.77	28 711	+40.3	96.5

Conclusions

Finally, for this study it can states that:

- ▶ Stabilized model and linear kinematic model allow a huge time saving but they don't lead to reliable results.
- ▶ Accelerated models represent a great solutions but the speed of stabilization have to be set opportunely.
- ▶ For further design purposes the accelerated model with $b = 20b_i$ represents a great solution.

THANK YOU FOR YOUR ATTENTION !

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-  Mahapatra, R. B., et al. "Mold behavior and its influence on quality in the continuous casting of steel slabs: Part i. Industrial trials, mold temperature

measurements, and mathematical modeling." Metallurgical Transactions B 22.6 (1991): 861-874.